

## Divergence of a vector field

### Flux

Given a vector field  $\vec{F}$  and an oriented surface  $S$  in space, we can think of the surface integral  $\iint_S \vec{F} \cdot d\vec{A}$  as a *flux*. In this interpretation, we think of  $\vec{F}$  as the velocity field of a fluid flow and think about the surface  $S$  as a rigid net in this flow. At each point on the surface, the components of  $\vec{F}$  tangent to the surface do not contribute to moving fluid across the net. Only the component of  $\vec{F}$  that is perpendicular to the surface is relevant. The area element vector  $d\vec{A}$  points perpendicular to the surface at each point so the dot product  $\vec{F} \cdot d\vec{A}$  gives us the component of  $\vec{F}$  perpendicular to the surface multiplied by the (infinitesimal) area  $dA$ . This is the rate at which fluid volume is flowing through the surface at each point. The surface integral  $\iint_S \vec{F} \cdot d\vec{A}$  is a summing up of these contributions and so gives us the total rate at which fluid volume flows across the surface.

### Divergence as flux density

Start with a vector field  $\vec{F}$  and focus on a point  $\mathcal{P}$  in the domain of the vector field. Imagine a small solid region that contains  $\mathcal{P}$ . (You can think of a rectangular box or a sphere if it helps to be specific about the shape.) We will use  $\Delta D$  to denote this solid region. Here  $\Delta$  doesn't mean "a small change in" but serves to remind us that the region is small. Let  $\Delta V$  be the volume of  $\Delta D$ . Let  $\Delta S$  be the closed surface that is the boundary of this solid region. Orient the area element vectors  $d\vec{A}$  for  $\Delta S$  to be pointing outward.

Both the flux  $\oiint_{\Delta S} \vec{F} \cdot d\vec{A}$  and the volume  $\Delta V$  will go to zero as we shrink the solid region  $\Delta D$  down to the point  $\mathcal{P}$ . However, the limit of the ratio

$$\frac{\oiint_{\Delta S} \vec{F} \cdot d\vec{A}}{\Delta V}$$

might exist. If so, this limit is the *volume flux density*. That is, the limit of the ratio is the flux per unit volume. We define the *divergence of the vector field  $\vec{F}$*  in terms of this flux density.

*The divergence of  $\vec{F}$  at  $\mathcal{P}$  is defined as the flux density at a point  $\mathcal{P}$ . That is,*

$$\operatorname{div} \vec{F}(\mathcal{P}) = \lim_{\Delta D \rightarrow \mathcal{P}} \frac{\oiint_{\Delta S} \vec{F} \cdot d\vec{A}}{\Delta V}$$

**Example 1**

Compute the divergence of the vector field  $\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$  at the origin  $(0,0,0)$ .

This vector points radially out from the origin so a convenient choice of a solid region  $\Delta D$  is a ball of radius  $R$  centered at the origin. The boundary  $\Delta S$  of this solid region is the sphere of radius  $R$  and the volume of the region is  $\Delta V = 4\pi R^3/3$ . We have previously computed the flux for this vector field through the sphere of radius  $R$  and found

$$\oiint_{\text{sphere}} \vec{F} \cdot d\vec{A} = 4\pi R^3.$$

So, we can form the ratio

$$\frac{\oiint_{\Delta S} \vec{F} \cdot d\vec{A}}{\Delta V} = \frac{4\pi R^3}{4\pi R^3/3} = 3$$

We thus have

$$\text{div } \vec{F}(0,0,0) = \lim_{\text{"}\Delta D \rightarrow \mathcal{P}\text{"}} \frac{\oiint_{\Delta S} \vec{F} \cdot d\vec{A}}{\Delta V} = \lim_{R \rightarrow 0} 3 = 3.$$

So, the flux density for  $\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$  at the origin  $(0,0,0)$  is positive. In a fluid flow interpretation, we can think of this as saying the fluid is being injected into the flow at  $(0,0,0)$ .

Computing divergence directly as a flux density is only feasible in cases with lots of symmetry. We now turn attention to a more efficient way to compute the divergence of a vector field.

**An expression for divergence in cartesian coordinates**

From the definition of divergence in terms of flux density, we learn what divergence tells us about the vector field. However, computing the divergence of a vector from this definition is difficult. We'll next look at getting an expression for the divergence in terms of partial derivatives with respect to cartesian coordinates.

Let the vector field  $\vec{F}$  be given in cartesian coordinates by

$$\vec{F}(x,y,z) = P(x,y,z)\hat{i} + Q(x,y,z)\hat{j} + R(x,y,z)\hat{k}.$$

We will compute the divergence using a rectangular box with one corner at the point  $\mathcal{P}(x,y,z)$  and the edges of the box parallel to the coordinate axes as shown in Figure 1. Let  $\Delta x$ ,  $\Delta y$ , and  $\Delta z$  be the edge lengths parallel to each of the coordinate axes. This rectangular box has six sides. Let  $\Delta \vec{A}_1, \Delta \vec{A}_2, \dots, \Delta \vec{A}_6$  be the area vectors for these six sides with the first two for the faces parallel to the  $yz$ -plane, the next two parallel to the  $xz$ -plane, and the last two parallel to the  $xy$ -plane. We then have, for example,  $\Delta \vec{A}_1 = -\Delta y \Delta z \hat{i}$ .

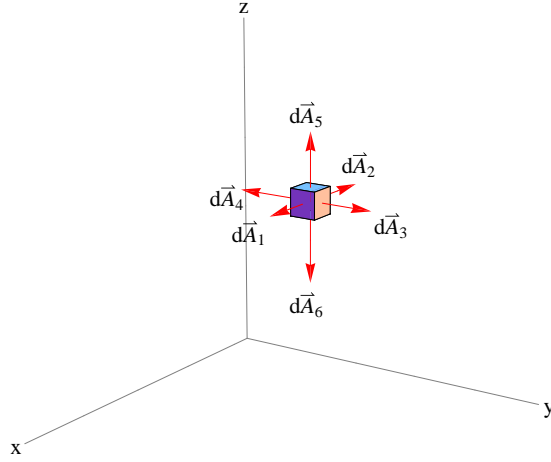


Figure 1. The rectangular box and normal vectors used in deriving a component expression for divergence.

For this geometry, the surface integral over the boundary of the box is approximated by a sum of six terms:

$$\oiint_{\Delta S} \vec{F} \cdot d\vec{A} \approx \vec{F}_1 \cdot \Delta\vec{A}_1 + \vec{F}_2 \cdot \Delta\vec{A}_2 + \vec{F}_3 \cdot \Delta\vec{A}_3 + \vec{F}_4 \cdot \Delta\vec{A}_4 + \vec{F}_5 \cdot \Delta\vec{A}_5 + \vec{F}_6 \cdot \Delta\vec{A}_6$$

with one term for each face of the box. In each term, the vector field is evaluated at a point on the corresponding face. For example, on the first face, we have

$$\vec{F}_1 \cdot \Delta\vec{A}_1 = -\vec{F}(x, y, z) \cdot \Delta y \Delta z \hat{i} = -P(x, y, z) \Delta y \Delta z.$$

For the opposite face, we have  $\Delta\vec{A}_2 = +\Delta y \Delta z \hat{i}$ , and

$$\vec{F}_2 \cdot \Delta\vec{A}_2 = \vec{F}(x + \Delta x, y, z) \cdot \Delta y \Delta z \hat{i} = P(x + \Delta x, y, z) \Delta y \Delta z.$$

Pairing the opposite sides parallel to the  $xz$ -plane and  $xy$ -plane in a similar fashion, we have

$$\begin{aligned} \oiint_{\Delta S} \vec{F} \cdot d\vec{A} \approx & [P(x + \Delta x, y, z) - P(x, y, z)] \Delta y \Delta z + [Q(x, y + \Delta y, z) - Q(x, y, z)] \Delta x \Delta z \\ & + [R(x, y, z + \Delta z) - R(x, y, z)] \Delta x \Delta y. \end{aligned}$$

To get the flux density at  $\mathcal{P}(x, y, z)$ , we divide by the volume  $\Delta V = \Delta x \Delta y \Delta z$  and take a limit as  $\Delta D \rightarrow \mathcal{P}$ . This is equivalent to  $\Delta x, \Delta y, \Delta z \rightarrow 0$ . The flux density

is thus

$$\begin{aligned}
 & \lim_{\Delta D \rightarrow \mathcal{P}} \frac{\oiint_{\Delta S} \vec{F} \cdot d\vec{A}}{\Delta V} \\
 &= \lim_{\Delta x, \Delta y, \Delta z \rightarrow 0} \frac{[P(x+\Delta x, y, z) - P(x, y, z)]\Delta y \Delta z + [Q(x, y+\Delta y, z) - Q(x, y, z)]\Delta x \Delta z + [R(x, y, z+\Delta z) - R(x, y, z)]\Delta x \Delta y}{\Delta x \Delta y \Delta z} \\
 &= \lim_{\Delta x, \Delta y, \Delta z \rightarrow 0} \left[ \frac{P(x+\Delta x, y, z) - P(x, y, z)}{\Delta x} + \frac{Q(x, y+\Delta y, z) - Q(x, y, z)}{\Delta y} + \frac{R(x, y, z+\Delta z) - R(x, y, z)}{\Delta z} \right] \\
 &= \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}.
 \end{aligned}$$

With this, we have the following result.

*In cartesian coordinates, the divergence of*

$$\vec{F} = P(x, y, z)\hat{i} + Q(x, y, z)\hat{j} + R(x, y, z)\hat{k}$$

*is given by*

$$\operatorname{div} \vec{F} = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

### Example 2

Compute the divergence of the vector field  $\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$ .

Using the coordinate expression for divergence, we have

$$\operatorname{div} \vec{F}(x, y, z) = \frac{\partial}{\partial x}[x] + \frac{\partial}{\partial y}[y] + \frac{\partial}{\partial z}[z] = 1 + 1 + 1 = 3.$$

So, the divergence of  $\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$  is equal to 3 at all points  $(x, y, z)$ . Note that this is consistent with what we got in Example 1 for the divergence of the same vector field at  $(0, 0, 0)$ . In a fluid flow interpretation, we can think of this as saying that fluid is being added to the flow at a certain rate at every point in space.

### The operator point of view

When we use the derivative operator  $d/dx$ , we think of it as meaning “take the derivative with respect to  $x$  of whatever follows”. So, for example, we read

$$\frac{d}{dx}[\sin x]$$

as “take the derivative with respect to  $x$  of  $\sin x$ ”. We record the result of doing this as

$$\frac{d}{dx}[\sin x] = \cos x.$$

In similar fashion, the operator  $\partial/\partial x$  means “take the partial derivative with respect to  $x$  of whatever follows”.

We now introduce the *vector operator*  $\vec{\nabla}$ . In cartesian coordinates, this operator is

$$\vec{\nabla} = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}.$$

If we apply this operator to a function  $f$  of three variables, we get

$$\vec{\nabla} f = \left( \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z} \right) [f] = \hat{i} \frac{\partial f}{\partial x} + \hat{j} \frac{\partial f}{\partial y} + \hat{k} \frac{\partial f}{\partial z} = \frac{\partial f}{\partial x} \hat{i} + \frac{\partial f}{\partial y} \hat{j} + \frac{\partial f}{\partial z} \hat{k}$$

This is just our familiar notation for the *gradient of  $f$* .

Now consider  $\vec{\nabla}$  acting on a vector field  $\vec{F} = P\hat{i} + Q\hat{j} + R\hat{k}$ . Since both  $\vec{\nabla}$  and  $\vec{F}$  are vector objects, one way to let  $\vec{\nabla}$  act on  $\vec{F}$  is to *dot* the two. This gives us

$$\vec{\nabla} \cdot \vec{F} = \left( \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z} \right) \cdot (P\hat{i} + Q\hat{j} + R\hat{k}) = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}.$$

Notice that this is precisely the *divergence of  $\vec{F}$* . So, we can write

$$\text{div } \vec{F} = \vec{\nabla} \cdot \vec{F}.$$

### Example 3

Compute the divergence of the vector field  $\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$  using the operator style.

Note that we are just repeating Example 2 using a different style. We have

$$\begin{aligned} \text{div } \vec{F} = \vec{\nabla} \cdot \vec{F} &= \left( \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z} \right) \cdot (x\hat{i} + y\hat{j} + z\hat{k}) \\ &= \frac{\partial}{\partial x}[x] + \frac{\partial}{\partial y}[y] + \frac{\partial}{\partial z}[z] = 1 + 1 + 1 = 3. \end{aligned}$$

The operator style will seem more useful once we use it in expressing the *curl* of a vector field.

### Problems: divergence of a vector field

1. Compute the divergence of the vector field  $\vec{F} = x\hat{i} + y\hat{j} + 0\hat{k}$  at the origin  $(0,0,0)$  directly as a flux density. For this, use a region  $\Delta D$  in the form of a solid cylinder centered at the origin of radius  $R$  and height  $H$ .

(a) Use a geometric argument to compute the flux  $\oiint_{\Delta S} \vec{F} \cdot d\vec{A}$  of the vector field through the cylinder surface.

(b) Write down the volume  $\Delta V$  of this cylinder.

(c) Form the ratio  $\oiint_{\Delta S} \vec{F} \cdot d\vec{A} / \Delta V$ .

(d) Evaluate the limit of the ratio in (c) as  $R \rightarrow 0$  and  $H \rightarrow 0$ .

For each of the following vector fields, compute the divergence. Evaluate the divergence at a few points and give an interpretation for each value.

2.  $\vec{F} = x\hat{i} + y\hat{j} + 0\hat{k}$

3.  $\vec{F} = -y\hat{i} + x\hat{j} + 0\hat{k}$

4.  $\vec{F} = x^2\hat{i} + y^2\hat{j} + z^2\hat{k}$

5.  $\vec{F} = z \sin(xy)\hat{i} + (x + y)\hat{j} + ze^x\hat{k}$

6.  $\vec{F} = \frac{x\hat{i} + y\hat{j}}{\sqrt{x^2 + y^2}}$

7.  $\vec{F} = \frac{x\hat{i} + y\hat{j}}{x^2 + y^2}$

8.  $\vec{F} = \frac{x\hat{i} + y\hat{j} + z\hat{k}}{\sqrt{x^2 + y^2 + z^2}}$

9.  $\vec{F} = \frac{x\hat{i} + y\hat{j} + z\hat{k}}{(x^2 + y^2 + z^2)^{3/2}}$